AMENDMENTS TO THE SPECIFICATION:

On page 22, line 4, please amend the paragraph as follows:

Fig. 6 shows the relationship between the inclination angle Θ_J of the bonded portion and the fracture strength of bonding. In the figure, each circle represents a case where no fracture is caused in the rolling process after bonding and each cross represents a case where fracture is caused. The result shows that the bonded portion is apt to fracture when the inclination angle Θ_J varies under different bonding conditions, including the amount of overlap of the shearing blades and the pressing stroke, the required strength of the bonded portion is higher when the inclination angle Θ_J is greater, that is, the bonded surface becomes inclined further. When the fracture strength becomes inclined further. When the fracture strength of the bonded portion is required to be around 3.0 kg/mm^2, the inclination angle Θ_J of the bonded portion that does not cause fracture is 75° or less.

On page 30, please amend the last paragraph bridging pages 30 and 31 as follows:

This shearing blade drive mechanism is constructed using almost the same drive mechanism as, for example, in a "Hitachi pendulum type frying shear" described in "Hitachi ~~Review~~ Hyouron" Vol. 61, No. 9 (1979-9). Variations are available to a synchronizing mechanism for synchronizing the shearing blades to the movement of the sheet bars. For example, it is possible to so

construct the mechanism that, after the shearing blades have bitten in the bars up until the shearing blades are separated upon completion of bonding, the shearing blades are allowed to naturally follow the bar movement and, when the shearing blades have been separated to a specified position, the shearing blades are returned to the original position by means of spring, for example. That is, it not always necessary that the shearing blades are synchronized with the main crankshaft.